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Spectral purity transfer with $5 \times 10^{-17}$ instability at 1 s using a multibranch Er:fiber frequency comb

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Abstract
In this work we describe the spectral purity transfer between a 1156 nm ultrastable laser and a 1542 nm diode laser by means of an Er:fiber multibranch comb. By using both the master laser light at 1156 nm and its second-harmonic at 578 nm, together with the 1542 nm slave laser, we investigate the residual noise between the main comb output, the octave-spanning output, and a wavelength conversion module including non-linear fibers, second-harmonic generation crystal and amplifiers. With an ultimate stability of the system at the level of $5 \times 10^{-17}$ at 1 s and accuracy of $3 \times 10^{-19}$, this configuration can sustain spectral transfer at the level required by the contemporary optical clocks with a simple and robust setup.

Keywords: optical frequency comb, multibranch Er:fiber comb, spectral purity transfer, ultrastable laser

(Some figures may appear in colour only in the online journal)
Benefits range from the search for new physics, to more ponderate considerations on the redefinition of the second in the SI, and future computations of the international atomic time based on optical clocks [21, 22].

In recent years, solid-state optical combs have been almost ubiquitously replaced by erbium-doped fiber (Er: fiber) devices. This is due to their higher reliability and robustness, which allow several days of continuous operation. However, their natural emission is in the 1–2 μm region. In order to cover the optical domain, dedicated wavelength conversion modules are exploited. In this way, it is possible to broaden the comb spectrum, preserving the phase-coherence with the fundamental comb and still provide adequate optical power per mode, at the cost of introducing additional noise to the system.

In this paper we present the spectral purity transfer between a 1156 nm ultrastable diode laser and a 1542 nm diode laser performed with an Er: fiber comb. The 1156 nm laser is used, after frequency doubling, as a clock laser in our Yb lattice clock at the Italian Metrology Institute (INRIM) [23]. Spectral transfer to a telecom wavelength will enable us to disseminate the frequency of the Yb standard to a number of research facilities, using the phase-stabilized ~2000 km optical fiber backbone we developed in Italy [24]. In addition, this setup will be used to generate the clock laser for the Sr optical clock under development in our laboratories [25].

We use the transfer oscillator technique proposed by Telle et al [26]. The beatnote between the 1542 nm slave laser and the comb is performed on the main comb output, which spans the 1.5–1.6 μm region. The 1156 nm master laser is detected on the broadband branch that spans the 1–2 μm range. The frequency-doubled master laser at 578 nm is detected on a few nm-wide dedicated branch. By using both the fundamental and frequency-doubled master laser we characterized the spectral transfer and the contribution of the separate comb branches without the need of a second, independent system. This measurement approach, which uses a single comb to study the spectral purity transfer, is different from that presented in previous works. Usually, two independent optical combs are used, one to perform the locking between the master and the slave lasers, the other to detect the out-of-loop beatnote [11–14].

In our work we separately considered all noise contributions to the spectral purity transfer, and we characterized both the electronics and the environmental noise on interferometers independently. We show that an Er: fiber optical comb used in the multibranch configuration achieves a residual frequency instability of 5 × 10⁻¹⁷(τ/s)⁻¹/² with accuracy of 3 × 10⁻¹⁹.

Even if single-branch combs achieve better performances [15, 16], a multibranch configuration offers higher power-per-mode in different spectral regions, which simplifies the measurement setup. Very recently, a method for rejecting the inter-branch comb noise has been demonstrated [27], which is promising when ultra high-accuracy has to be guaranteed. However, multibranch configuration still offers adequate performances with a simple and robust system.

2. Experimental setup

2.1. The optical frequency comb

The optical comb used for the spectral purity transfer is a commercial femtosecond Er: fiber comb. It is based on passive mode-locking through non-linear polarization rotation. The main output is centered at 1560 nm and spans 100 nm, the repetition rate f_{rep} is 250 MHz.

The main comb output is split in three independent branches (see figure 1). The first branch is a fraction of the 1560 nm output of the femtosecond mode-locked laser. The second branch consists in an erbium-doped fiber amplifier (EDFA) followed by a highly non-linear fiber (HNLF) that generates an octave-spanning spectrum between 1 μm and 2 μm. This branch is used to detect the carrier-envelope offset frequency f_{c-e} through the f − 2f interferometer, with 2.5 mW power output available for other measurements. The third branch is a wavelength conversion module operating at 578 nm. It consists in a second EDFA and a wavelength-shifting fiber that produces 1156 nm radiation. Then, the 1156 nm light is frequency-doubled with a bulk periodically poled lithium niobate (PPLN) crystal. In this way a 1.1 nm-wide output at 578 nm is obtained, with an average power of 5 mW and a power per tooth of 1 μW. The spectrum of the f − 2f and the 578 nm branches can be tailored by adjusting the current of the 980 nm pump diode lasers that act on the EDFA (four pump lasers for each EDFA).

The repetition rate and the offset frequency are stabilized to a hydrogen maser by means of two phase-locked-loops (PLLS). The former acts on the cavity length by moving one of the cavity mirrors using a piezo, on a bandwidth of 3.5 kHz. The second acts on the power of the femtosecond Er: fiber oscillator pump laser to modify intracavity dispersion. In principle, the spectral transfer does not require a tight stabilization of the comb repetition rate and offset frequency, since their noise is canceled out [26]. In practice, however, they are locked to prevent long-term drifts that might bring beatnotes outside the filters’ bandwidth.

The comb and all the optical interferometers developed for the beatnotes’ detection are placed in a foam enclosure to reduce the effect of air currents and temperature variations on the fiber.

2.2. Laser sources and beatnote detection

The master laser used in our experiment is a 1156 nm diode laser, frequency-doubled in a waveguide-PPLN crystal to 578 nm. This is used to probe the ¹S₀ − ¹P₀ clock transition at 578 nm of the ¹⁷¹Yb optical lattice clock [23]. The doubling stage produces up to 9 mW of 578 nm radiation, while 4 mW of 1156 nm are still available after the crystal waveguide. Part of the 578 nm radiation is used to stabilize the laser to a 10 cm cavity made of ultra-low expansion glass through the Pound–Drever–Hall technique [28]. The residual laser frequency instability is 2 × 10⁻¹⁵ at 1 s averaging time, with a drift of 0.15 Hz s⁻¹. 1 mW of the 1156 nm laser is detected on the f − 2f-branch of the comb. The beatnote reaches up to 37 dB
of signal-to-noise ratio (SNR) in a 100kHz resolution band-
width (RBW). 600 µW of 578 nm light are beaten with the
578 nm comb branch, producing a beatnote signal with 35 dB
SNR in a 100kHz RBW. The 1156 nm and 578 nm radia-
tions are sent to the optical comb through polarization-maintaining
(PM) Doppler-stabilized optical fibers [29]. Both beatnotes
are detected through free-space interferometers. An external
cavity diode laser at 1542 nm with output power of 9 mW
[30] and linewidth <10kHz is phase-locked to the master
laser at 1156 nm using the transfer oscillator scheme. 100 µW
of its output power are beaten to the main comb output at
1560 nm through an all-fiber-coupled optical interferometer.
The detected beatnote has a SNR of 40 dB in a 100kHz RBW.

We use a transfer oscillator scheme to obtain a beatnote
between the 1542 nm laser and the 1156 nm laser [26]. This
is stabilized by a PLL that acts on an acousto-optic modulator
with a bandwidth of 60kHz, and on the diode laser current.
The slave laser is used without any pre-stabilization. To
achieve cycles-slip free operation for several hours with minimal adjustment of
the comb amplifiers pump power, and do not need tracking
oscillators.

2.3. Transfer oscillator setup

Figure 2 shows the electronic setup we developed for gener-
ating the virtual beatnote between the 1156 nm master laser
and the 1542 nm slave laser (in-loop beatnote \( f_{m} \)), which is
used for the PLL.

Being \( \nu_{1156} \) and \( \nu_{1542} \) the absolute frequencies of the CW
lasers, \( f_{b,1156} \) and \( f_{b,1542} \) the beatnotes between the CW
lasers and the comb, \( m_{1156} \) and \( m_{1542} \) the indexes of the comb teeth
to which the lasers are beaten, then the in-loop beatnote can be writ-
ten as:

\[
f_{m} = \frac{1}{4} \frac{m_{1156}}{m_{1542}} f_{b,1156} - \frac{1}{4} f_{b,1542}
\]

\[
= \frac{1}{4} \left( \nu_{1156} - \frac{m_{1542}}{m_{1156}} \nu_{1542} \right),
\]

where \( f_{b,1156} \) and \( f_{b,1542} \) indicate the \( f_{0} \)-free signals \( f_{b,1156} = f_{0} + f_{b,1156} \) and \( f_{b,1542} = f_{0} + f_{b,1542} \), which are obtained using
frequency mixers.

The scaling factor \( 1/4 \times m_{1542}/m_{1156} \) is applied to \( f_{b,1156} \)
by using a direct digital synthesizer (DDS). The factor of \( 1/4 \)
is used as with the original teeth ratio \( m_{1542}/m_{1156} \sim 0.75 \)
the DDS output frequency would be above the DDS Nyquist
frequency. A second DDS (DDS2 in figure 2) or a prescaler is
used to scale \( f_{b,1542} \) accordingly. We use Analog Devices
AD9912 DDSs, which have a 14-bit digital-to-analog con-
verter and 4 MHz resolution. We verified that the DDSs do not
introduce cycles slips as long as the SNR on the beatnotes and
on \( f_{0} \) is >33 dB in a 100kHz RBW.

The electronic scheme has been designed to be easily
adapted to any value of the beatnotes with minor changes.
Several local oscillators (LOs) are used to match the band-
pass filters and have been omitted in equation (1) for the sake
of clarity. The red elements in figure 2 indicate the only com-
ponents that need to be adjusted when using different lasers,
i.e. the frequency of the LOs and the band-pass filters at the
output of the DDSs.

3. Characterization

To fully characterize the spectral transfer and the inter-branch
noise, we performed the following measurements: first, we
characterized the noise between the 1.56 µm-branch, the
\( f - 2f \)-branch and the 578 nm-branch. Then, we compared the
1542 nm slave laser, phase-locked to the 1156 nm master laser,
to the second harmonic of the latter at 578 nm. Measurements
were conducted using a digital phasemeter with 1 MHz band-
width and an eight-channel, dead-time free synchronous fre-
quency counter in the averaging configuration with 1 s gate
time. The two measurement approaches are complementary:
the former allowed computation of phase noise spectra, suited
to inspect fundamental noise processes at high Fourier fre-
quencies. The latter has been used to calculate the frequency
instability in terms of Allan deviation, that better quantifies
the long-term behavior of the system. Thanks to the leverage
between RF and optical domain, the counter resolution did not
limit the measurement at the \( 2 \times 10^{-20} \) level.

3.1. \( f - 2f \) and 1.56µm branches noise

We detected the beatnotes between the same laser at 1542 nm
and the comb in the \( f - 2f \) and 1.56 µm branches and analyzed
the frequency noise of their difference. Figure 3 (green curve)
shows the corresponding power spectral density, that quantifi-
cies the residual frequency noise between the two branches.
The residual instability is shown in terms of overlapping Allan
deviation by the green curve in figure 4, which is in agreement
with the observed spectrum, considering that the equivalent
measurement bandwidth of the counter is 0.5 Hz.

We note that the \( f - 2f \) branch includes an EDFA and a
HNLF to achieve the octave-spanning broadening, while the
1.56 µm branch does not include additional components.
Therefore, the reported curves represent the noise of EDFA,
HNFL and other uncommon fibers.

3.2. \( f - 2f \) and 578nm branches noise

We measured the frequency ratio between the 1156 nm master
laser beaten to the \( f - 2f \) branch and its 578 nm second har-
monic beaten to the 578 nm branch \( (f_{b,578}) \). We calculated the
virtual beatnote between the two lasers by post-processing the
simultaneous counting of \( f_{0} \), \( f_{b,1156} \) and \( f_{b,578} \).

For a better inspection of high-frequency noise we also
generate this beatnote physically by implementing the transfer
oscillator scheme shown in figure 5. Note that if the comb
branch used for the beatnote detection is generated from a fre-
quency-doubling process, as in the case of the 578 nm-branch,
the second harmonic of \( f_{0} \) is used to produce the \( f_{0} \)-free beat-
note instead of the fundamental tone. This is achieved by
adding a multiplier after \( f_{0} \) (‘\( 2 \times \)’ box in figure 5). Therefore,
the \( f_{0} \)-free beatnote in this case is \( f_{b,578} = f_{b,578} + 2f_{0} \).

\[
\nu_{1156} \quad \text{and} \quad \nu_{1542} \quad \text{the absolute frequencies of the CW}
\text{lasers,} \quad f_{b,1156} \text{and} \quad f_{b,1542} \quad \text{the beatnotes between the CW}
\text{lasers and the comb,} \quad m_{1156} \quad \text{and} \quad m_{1542} \quad \text{the indexes of the comb teeth}
\text{to which the lasers are beaten, then the in-loop beatnote can be writ-
ten as:}
\]

\[
= \frac{1}{4} \frac{m_{1156}}{m_{1542}} f_{b,1156} - \frac{1}{4} f_{b,1542}
\]

\[
= \frac{1}{4} \left( \nu_{1156} - \frac{m_{1542}}{m_{1156}} \nu_{1542} \right),
\]

where \( f_{b,1156} \) and \( f_{b,1542} \) indicate the \( f_{0} \)-free signals \( f_{b,1156} = f_{0} + f_{b,1156} \) and \( f_{b,1542} = f_{0} + f_{b,1542} + f_{0} \), which are obtained using
frequency mixers.

The scaling factor \( 1/4 \times m_{1542}/m_{1156} \) is applied to \( f_{b,1156} \)
by using a direct digital synthesizer (DDS). The factor of \( 1/4 \)
is used as with the original teeth ratio \( m_{1542}/m_{1156} \sim 0.75 \)
the DDS output frequency would be above the DDS Nyquist
frequency. A second DDS (DDS2 in figure 2) or a prescaler is
used to scale \( f_{b,1542} \) accordingly. We use Analog Devices
AD9912 DDSs, which have a 14-bit digital-to-analog con-
verter and 4 MHz resolution. We verified that the DDSs do not
introduce cycles slips as long as the SNR on the beatnotes and
on \( f_{0} \) is >33 dB in a 100kHz RBW.

The electronic scheme has been designed to be easily
adapted to any value of the beatnotes with minor changes.
Several local oscillators (LOs) are used to match the band-
pass filters and have been omitted in equation (1) for the sake
of clarity. The red elements in figure 2 indicate the only com-
ponents that need to be adjusted when using different lasers,
Figures 3 and 4 show the corresponding frequency noise and instability (yellow curves). In these measurements, both comb outputs are directly combined with the laser light through free-space paths. This configuration leads to a long-term instability dominated by a white frequency noise process for $\tau > 10$ s in agreement with the observed spectrum, and achieves an ultimate level of $3 \times 10^{-19}$ at 10000 s. No offset was observed at this level. This puts an upper limit to the frequency instability of conversion between fundamental and second harmonic radiation at 578 nm in our crystal and phase-stabilized fiber links that bring the 1156 nm and the 578 nm light to the comb. We also note that a flicker frequency...
Figure 3. Frequency noise spectrum of the comparison between the $f - 2f$ and 578 nm branches via spectral purity transfer at 1542 nm laser (blue), of the in-loop beatnote $f_{in}$ between the 1542 nm laser and the 1156 nm laser (red), of the 578 nm branch with respect to the to the $f - 2f$-branch (yellow), of the 1.56 µm branch with respect to the $f - 2f$-branch (green). All the spectra are reported in the 1542 nm spectral window.

Figure 4. Fractional stability measurements in terms of Allan deviation (Adev). Green: $f - 2f$ and 1.56 µm branches noise measured by beating the same 1542 nm laser on the two branches. Blue: $f - 2f$ and 578 nm branches noise via spectral purity transfer at 1542 nm. Yellow: frequency ratio measurement $\nu_{578}/\nu_{1156}$. 
instability at the level of $5 \times 10^{-18}$ was observed when the $f - 2f$ comb output traveled over a 1 m uncompensated PM fiber. For that reason, we replaced uncompensated fiber paths with free-space paths in our comb wherever possible.

3.3. $f - 2f$ and 578 nm branches via spectral purity transfer at 1542 nm

We measured the virtual beatnote between the 578 nm and the 1542 nm lasers when the latter was phase-locked to the 1156 nm laser. The implementation scheme is shown in figure 5 (see labels in brackets). Figures 3 and 4 show the corresponding frequency noise and instability (blue curves). The Allan deviation achieves the $5 \times 10^{-17}$ level at 1 s, in agreement with the observed spectrum, and decreases to the ultimate $3 \times 10^{-19}$ level after 10000 s. Noise sources that affect this beatnote include the residual noise between the $f - 2f$ and the 578 nm comb branches, the noise of the PLL between the 1542 nm and the 1156 nm laser, the noise of the phase-stabilized fibers which bring the 1156 nm and the 578 nm light to the comb, and possibly the noise of the second harmonic generation at 578 nm. The noise of the 1.56 μm branch is rejected as it is common between the two transfer schemes.

3.4. Comments

From the measurements described in sections 3.1–3.3, we can quantify the noise of the three branches and the spectral transfer between our 1156 nm and 1542 nm lasers. From a comparison of the spectra in figure 3, it is evident that the measurements involving the 578 nm branch have a higher noise at Fourier frequencies between $10^{-1}$ Hz and 100 Hz. This behavior can be seen as well from the comparison of the short term frequency instability of the three measurements. This is attributed to the phase-stabilization circuits that independently stabilize the fibers paths of the 1156 nm and 578 nm lasers to the comb [29]. The performances of the spectral transfer between the 1156 nm and the 1542 nm laser are represented by a combination of the results of the tests described in sections 3.1 and 3.3. The inter-branch noise between the 1.56 μm and $f - 2f$ branches, shown by the green curve in figure 3, quantifies the noise of EDFA, HNLF and other uncompensated fibers. The noise excess corresponding to the slope deviation from white frequency noise below 1 Hz Fourier frequencies is attributed to thermal effects in the laboratory. The blue curve in the figure includes the inter-branch noise between the 578 nm and $f - 2f$ branches and the noise of the PLL as well. As it is dominant over the inter-branch comb throughout the full Fourier spectrum, we can consider it as the upper limit to the spectral transfer noise. At Fourier frequencies $>100$ Hz, the noise is limited by the in-band rejection of the PLL, hence by the locking bandwidth, as can be noted by comparing the blue curve with respect to the in-loop beatnote $f_n$ noise (red curve). Further reduction in the high-frequency noise could be gained with higher bandwidth or with low-noise diode lasers. At lower frequencies, the inter-branch noise emerges. The measurement sensitivity is here limited by the fiber-stabilization loops; the lower limit to the noise is represented by the green curve, i.e. the inter-branch noise between the 1.56 μm and the $f - 2f$ branches. The corresponding fractional frequency instability is $5 \times 10^{-17}$ at 1 s. We note that a residual sensitivity to the external environment is still observed around 400 s, which is due to the air conditioning in our laboratory. Even in the worst case, however, the ultimate stability achieves the level of $3 \times 10^{-19}$ and no frequency offset has been observed at this level.

4. Discussion and conclusions

We performed the spectral purity transfer between the 1156 nm ultrastable laser used to probe the clock transition of the $^{171}$Yb optical lattice clock and a 1542 nm diode laser,
In this way, we put an upper limit to the transfer instability the spectral transfer without using a second reference comb. This in turn can thus exploit the \( f - 2f \) branch of the master laser, and a dedicated wave-length conversion module for reaching the spectral region of interest for the experiment. Here, we characterized a module at 578 nm, however the physical components are the same as for other wavelength-dedicated modules.

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